Notes

- ◆ Final Project
 - Please contact me this week with ideas, so we can work out a good topic

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Reduced Coordinates

- Constraint methods from last class involved adding forces, variables etc. to remove degrees of freedom
- ◆ Inevitably have to deal with drift, error, ...
- Instead can (sometimes) formulate problem to directly eliminate degrees of freedom
 - Give up some flexibility in exchange for eliminating drift, possibly running a lot faster
- "Holonomic constraints": if we have n true degrees of freedom, can express current position of system with n variables
 - Rigid bodies: centre of mass and Euler angles
 - Articulated rigid bodies: base link and joint angles

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Finding the equations of motion

- Unconstrained system state is x, but holonomic constraints mean x=x(q)
 - The vector q is the "generalized" or "reduced" coordinates of the system
 - dim(q) < dim(x)
- Suppose our unconstrained dynamics are

$$\frac{d}{dt}(Mv) = F$$

- Could include rigid bodies if M includes inertia tensors as well as standard mass matrices
- What will the dynamics be in terms of q?

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Principle of virtual work

- ◆ Differentiate x=x(q): $v = \frac{\partial x}{\partial q}\dot{q}$
- ♦ That is, legal velocities are some linear combination of the columns of ∂x
 - (coefficients of that combination $\overline{\partial q}$ are just dq/dt)
- Principle of virtual work: constraint force must be orthogonal to this space

$$\frac{\partial x}{\partial q}^T F_{\text{constraint}} = 0$$

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Equation of motion

• Putting it together, just like rigid bodies,

$$\frac{\partial x}{\partial q}^{T} \frac{\partial}{\partial t} \left(M \frac{\partial x}{\partial q} \dot{q} \right) = \frac{\partial x}{\partial q}^{T} F$$

$$\left(\frac{\partial x}{\partial q}^{T} M \frac{\partial x}{\partial q} \right) \ddot{q} + \frac{\partial x}{\partial q}^{T} \dot{M} \frac{\partial x}{\partial q} \dot{q} + \frac{\partial x}{\partial q}^{T} M \frac{\partial v}{\partial q} \dot{q} = \frac{\partial x}{\partial q}^{T} F$$

- Note we get a matrix times second derivatives, which we can invert at any point for second order time integration
- Generalized forces on right hand side
- Other terms are pseudo-forces (e.g. Coriolis, centrifugal force, ...)

Generalized Forces

- Sometimes the force is known on the system, and so the generalized force just needs to be calculated
 - E.g. gravity
- But often we don't care what the true force is, just what its effect is: directly specify the generalized forces
 - · E.g. joint torques

Cleaning things up

- Equations are rather messy still
- ◆ Classical mechanics has spent a long time playing with the equations to make them nicer
 - And extend to include non-holonomic constraints for example
- Let's look at one of the traditional approaches: Lagrangian mechanics

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Setting up Lagrangian Equations

- For simplicity, assume we model our system with N point masses, positions controlled by generalized coordinates
- We'll work out equations via kinetic energy
- As before F_{constraint} + F = Ma
 Using principle of virtual work, can eliminate Using principle of virtual $\frac{\partial x}{\partial q}^T F = \frac{\partial x}{\partial q}^T Ma$

◆ Equation j is just

$$\sum_{i=1}^{N} \frac{\partial \overline{x}_{i}}{\partial q_{j}} \cdot \vec{F}_{i} = \sum_{i=1}^{N} m_{i} \vec{a}_{i} \cdot \frac{\partial \overline{x}_{i}}{\partial q_{j}}$$

Introducing Kinetic Energy

$$\begin{split} \sum_{i=1}^{N} m_{i} \overline{a}_{i} \cdot \frac{\partial \overline{x}_{i}}{\partial q_{j}} &= \sum_{i=1}^{N} m_{i} \left(\frac{d}{dt} \left(\overline{v}_{i} \cdot \frac{\partial \overline{x}_{i}}{\partial q_{j}} \right) - \overline{v}_{i} \cdot \frac{d}{dt} \frac{\partial \overline{x}_{i}}{\partial q_{j}} \right) \\ &= \sum_{i=1}^{N} m_{i} \left(\frac{d}{dt} \left(\overline{v}_{i} \cdot \frac{\partial \overline{v}_{i}}{\partial \dot{q}_{j}} \right) - \overline{v}_{i} \cdot \frac{\partial \overline{v}_{i}}{\partial q_{j}} \right) \\ &= \sum_{i=1}^{N} m_{i} \left(\frac{d}{dt} \left(\frac{1}{2} \frac{\partial}{\partial \dot{q}_{j}} |v_{i}|^{2} \right) - \frac{1}{2} \frac{\partial}{\partial q_{j}} |v_{i}|^{2} \right) \\ &= \frac{d}{dt} \left(\frac{\partial}{\partial \dot{q}_{j}} \sum_{i=1}^{N} \frac{1}{2} m_{i} |v_{i}|^{2} \right) - \frac{\partial}{\partial q_{j}} \sum_{i=1}^{N} \frac{1}{2} m_{i} |v_{i}|^{2} \\ &= \frac{d}{dt} \frac{\partial T}{\partial \dot{q}_{j}} - \frac{\partial T}{\partial q_{j}} \end{split}$$
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Lagrangian Equations of Motion

Label the j'th generalized force

$$f_{j} = \sum_{i=1}^{N} \vec{F}_{i} \cdot \frac{\partial \vec{x}_{i}}{\partial q_{j}}$$

◆ Then the Lagrangian equations of motion are (for j=1, 2, ...):

$$f_{j} = \frac{d}{dt} \frac{\partial T}{\partial \dot{q}_{j}} - \frac{\partial T}{\partial q_{j}}$$

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Potential Forces

 ◆ If force on system is the negative gradient of a potential W (e.g. gravity, undamped springs, ...) then further simplification: $f_j = \sum_{i=1}^N \bar{F}_i \cdot \frac{\partial \bar{x}_i}{\partial q_j} = \sum_{i=1}^N -\frac{\partial W}{\partial \bar{x}_i} \frac{\partial \bar{x}_i}{\partial q_j} = -\frac{\partial W}{\partial q_j}$

$$f_{j} = \sum_{i=1}^{N} \vec{F}_{i} \cdot \frac{\partial \vec{x}_{i}}{\partial a_{i}} = \sum_{i=1}^{N} -\frac{\partial W}{\partial \vec{x}_{i}} \frac{\partial \vec{x}_{i}}{\partial a_{i}} = -\frac{\partial W}{\partial a_{i}}$$

Plugging this in

$$-\frac{\partial W}{\partial q_j} = \frac{d}{dt} \frac{\partial T}{\partial \dot{q}_j} - \frac{\partial T}{\partial q_j} \implies \frac{d}{dt} \frac{\partial T}{\partial \dot{q}_j} = \frac{\partial (T - W)}{\partial q_j}$$

◆ Defining the Lagrangian L=T-W.

$$\frac{d}{dt}\frac{\partial L}{\partial \dot{q}_{j}} = \frac{\partial L}{\partial q_{j}}$$

Implementation

- For any kind of reasonably interesting articulated figure, expressions are truly horrific to work out by hand
- Use computer: symbolic computing, automatic differentiation
- Input a description of the figure
- Program outputs code that can evaluate terms of differential equation
- Use whatever numerical solver you want (e.g. Runge-Kutta)
- Need to invert matrix every time step in a numerical integrator
 - · Gimbal lock...

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Fluid mechanics

Fluid mechanics

- We already figured out the equations of motion for continuum mechanics $\rho \ddot{x} = \nabla \cdot \sigma + \rho g$
- ◆ Just need a constitutive model

$$\sigma = \sigma(x, t, \varepsilon, \dot{\varepsilon})$$

- We'll look at the constitutive model for "Newtonian" fluids
 - Remarkably good model for water, air, and many other simple fluids
 - · Only starts to break down in extreme situations, or more complex fluids (e.g. viscoelastic substances)

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Inviscid Euler model

- Inviscid=no viscosity
- · Great model for most situations
 - Numerical methods end up with viscosity-like error terms anvwavs...
- Constitutive law is very simple: $\sigma_{ii} = -p\delta_{ii}$
 - New scalar unknown: pressure p
 - Barotropic flows: p is just a function of density (e.g. perfect gas law $p=k(\rho-\rho_0)+p_0$ perhaps)
 - For more complex flows need heavy-duty thermodynamics: an equation of state for pressure, equation for evolution of internal energy (heat), ...

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Lagrangian viewpoint

- We've been working with Lagrangian methods so far
 - · Identify chunks of material. track their motion in time, differentiate world-space position or velocity w.r.t. material coordinates to get forces
 - In particular, use a mesh connecting particles to approximate derivatives (with FVM or FEM)
- Bad idea for most fluids
 - [vortices, turbulence]
 - · At least with a fixed mesh...

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Eulerian viewpoint

- ◆ Take a fixed grid in world space, track how velocity changes at a point
- Even for the craziest of flows, our grid is always
- (Usually) forget about object space and where a chunk of material originally came from
 - Irrelevant for extreme inelasticity
 - Just keep track of velocity, density, and whatever else is needed

Conservation laws

- Identify any fixed volume of space
- ◆ Integrate some conserved quantity in it (e.g. mass, momentum, energy, ...)
- Integral changes in time only according to how fast it is being transferred from/to surrounding space
 - Called the flux

 $\frac{\partial}{\partial t} \int_{\Omega} q = -\int_{\partial \Omega} f(q) \cdot n$

• [divergence form] $q_r + \nabla \cdot f = 0$

Conservation of Mass

- Also called the continuity equation (makes sure matter is continuous)
- Let's look at the total mass of a volume (integral of density)
- Mass can only be transferred by moving it: flux must be ρu

$$\frac{\partial}{\partial t} \int_{\Omega} \rho = -\int_{\partial \Omega} \rho u \cdot n$$
$$\rho_t + \nabla \cdot (\rho u) = 0$$

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Material derivative

- A lot of physics just naturally happens in the Lagrangian viewpoint
 - E.g. the acceleration of a material point results from the sum of forces on it
 - How do we relate that to rate of change of velocity measured at a fixed point in space?
 - Can't directly: need to get at Lagrangian stuff somehow
- ullet The material derivative of a property q of the material (i.e. a quantity that gets carried along with the fluid) is \underline{Dq}

 \overline{Dt}

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Finding the material derivative

 Using object-space coordinates p and map x=X(p) to world-space, then material derivative is just

$$\frac{D}{Dt}q(t,x) = \frac{d}{dt}q(t,X(t,p))$$

$$= \frac{\partial q}{\partial t} + \nabla q \cdot \frac{\partial x}{\partial t}$$

$$= a + u \cdot \nabla q$$

 Notation: u is velocity (in fluids, usually use u but occasionally v or V, and components of the velocity vector are sometimes u,v,w)

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Compressible Flow

- In general, density changes as fluid compresses or expands
- When is this important?
 - Sound waves (and/or high speed flow where motion is getting close to speed of sound - Mach numbers above 0.3?)
 - Shock waves
- Often not important scientifically, almost never visually significant
 - Though the effect of e.g. a blast wave is visible! But the shock dynamics usually can be hugely simplified for graphics

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Incompressible flow

- So we'll just look at incompressible flow, where density of a chunk of fluid never changes
 - Note: fluid density may not be constant throughout space - different fluids mixed together...
- That is, Dρ/Dt=0

Simplifying

• Incompressibility: $\frac{D\rho}{Dt} = \rho_t + u \cdot \nabla \rho = 0$

Conservation of mass:

$$\rho_t + \nabla \cdot (\rho u) = 0$$

 $ρ_t + ∇ρ \cdot u + ρ∇ \cdot u = 0$ ◆ Subtract the two equations, divide by ρ:

$$\nabla \cdot u = 0$$

- υ Incompressible == divergence-free velocity
 - Even if density isn't uniform!

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Conservation of momentum

• Short cut: in $\rho \ddot{x} = \nabla \cdot \sigma + \rho g$

use material derivative:

$$\rho \frac{Du}{Dt} = \nabla \cdot \sigma + \rho g$$
$$\rho (u_t + u \cdot \nabla u) = \nabla \cdot \sigma + \rho g$$

- Or go by conservation law, with the flux due to transport of momentum and due to stress:
 - · Equivalent, using conservation of mass

$$(\rho u)_t + \nabla \cdot (u\rho u - \sigma) = \rho g$$

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Inviscid momentum equation

♦ Plug in simplest consitutive law (σ =-p δ) from before to get

$$\rho(u_t + u \cdot \nabla u) = -\nabla p + \rho g$$
$$u_t + u \cdot \nabla u + \frac{1}{\rho} \nabla p = g$$

 Together with conservation of mass: the Euler equations

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Incompressible inviscid flow

- ♦ So the equations are: $u_t + u \cdot \nabla u + \frac{1}{\rho} \nabla p = g$
- ◆ 4 equations, 4 unknowns (u, p)
- Pressure p is just whatever it takes to make velocity divergence-free
- ◆ In fact, incompressibility is a hard constraint; div and grad are transposes of each other and pressure p is the Lagrange multiplier
 - Just like we figured out constraint forces before...

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Pressure solve

◆ To see what pressure is, take divergence of momentum equation

$$\begin{split} \nabla \cdot \left(u_{t} + u \cdot \nabla u + \frac{1}{\rho} \nabla p - g \right) &= 0 \\ \nabla \cdot \left(\frac{1}{\rho} \nabla p \right) &= -\nabla \cdot \left(u_{t} + u \cdot \nabla u - g \right) \end{split}$$

- For constant density, just get Laplacian (and this is Poisson's equation)
- Important numerical methods use this approach to find pressure

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Projection

Note that ∇•u_t=0 so in fact

$$\nabla \cdot \frac{1}{\rho} \nabla p = -\nabla \cdot \left(u \cdot \nabla u - g \right)$$

- υ After we add $\nabla p/\rho$ to u• ∇u , divergence must be zero
- So if we tried to solve for additional pressure, we get zero
- υ Pressure solve is linear too
- υ Thus what we're really doing is a **projection** of u•∇u-g onto the subspace of divergence-free functions: $u_{+}+P(u\cdot\nabla u-g)=0$